

## Power Supply IC Series for TFT-LCD Panels

# **Automotive Panel Power Management IC**

## **BD81842MUV-M**

## General Description

The BD81842MUV-M is a power management IC for TFT-LCD panels which are used in car navigation, in-vehicle center panel, and instrument cluster. Incorporates high-power FET with low on resistance for large currents that employ high-power packages, thus driving large current loads while suppressing the generation of heat. A charge pump controller is incorporated as well, thus greatly reducing the number of application components. Also Gate Shading Function is included.

#### Key Specifications

- Input voltage range : 2.0V to 5.5V
- AVDD Output voltage range : 6.0V to 18V
- SRC Output voltage range : 12V to 34V
- VCOM Output current : 200mA (Typ.)
- Oscillator Frequency : 2.1MHz (Typ.)
- -Operating temperature range : -40°C to +105°C

#### Special Characteristics

- FB Regulation voltage :  $\pm 3\%$  (Ta=-40~105°C)
- ±10.5% (Ta=-40~105°C) **Oscillator Frequency :**

#### Typical Application Circuit (TOP VIEW)

#### Applications

TFT-LCD Panels which are used in car navigation, in-vehicle center panel, and instrument cluster.

#### Features

- AEC-Q100 Qualified<sup>(Note 1)</sup>
- Boost DC/DC converter; 18 V / 2.5 A switch current.
- Switching frequency: 2.1 MHz
- Operational Amplifier (short current 200mA)
- Incorporates Positive / Negative Charge-pump Controllers.
- Gate Shading Function
- Protection circuits:
  - Under Voltage Lockout
  - Protection Circuit
    - Thermal Shutdown Circuit (Latch Mode)
  - Over Current Protection Circuit (AVDD) Timer Latch Mode Short Circuit Protection (AVDD SRC /VGL)

Over / Under Voltage Protection Circuit for Boost DC/DC Output

No SCP time included (185ms from UVLO-off) (Note1: Grade 2)

## Package

VQFN24SV4040

W(Typ.) x D(Typ.) x H(Max.) 4.0mm x 4.0mm x 1.0mm



Figure 1. Application Circuit

OProduct structure : Silicon monolithic integrated circuit OThis product is not designed for protection against radioactive rays

## Contents

General Description	1
<ul> <li>General Description</li> <li>Key Specifications</li> </ul>	1
Special Characteristics	1
Applications	1
Features	1
Pin Configuration	3
<ul> <li>Pin Descriptions</li> <li>Block Diagram</li> </ul>	3
Block Diagram	4
Main Block Function	5
Absolute Maximum Ratings	
Thermal Resistance	
Recommended Operating Range	
Electrical characteristics	
Electrical characteristic curves	
Application Example	15
Power Sequence	16
Protect Operation	
Reset Function	
Gate Shading Function	18
<ul> <li>How to select parts of application</li> <li>PCB Layout Guide</li> </ul>	19
●I/O Equivalent Circuit Diagrams	
Operation Notes	
Ordering Information	29
<ul> <li>Marking Diagrams</li> <li>Physical Dimension, Tape and Reel Information</li> </ul>	29
Revision History	31

## ●Pin Configuration (TOP VIEW)



#### Pin Descriptions

Pin No.	Pin Name	Function
1	INP	VCOM Amplifier input +
2	INN	VCOM Amplifier input -
3	VCOM	VCOM Amplifier output
4	AGND1	Ground
5	AVDD	Supply voltage input for VCOM, charge pump
6	DRP	Drive pin of the positive charge pump
7	DRN	Drive pin of the negative charge pump
8	CTL	High voltage switch control pin
9	RST	Open drain reset output
10	FBP	Positive charge pump feed back
11	FBN	Negative charge pump feed back
12	VREF	Internal Reference voltage output
13	VIN	Supply voltage input for PWM
14	AGND2	Ground
15	RSTIN	Reset comparator input
16	COMP	BOOST Error amplifier output
17	FB	BOOST Error amplifier input
18	PGND1	BOOST FET ground
19	PGND2	BOOST FET ground
20	SW	BOOST FET Drain
21	RE	Gate High voltage Fall set pin
22	GSOUT	Gate High voltage output set pin
23	SRC	Gate High voltage input set pin
24	DLY	GSOUT Delay Adjust pin

## Block Diagram





## Main Block Function

 Boost Converter A controller circuit for DC/DC boosting. The switching duty is controlled so that the feedback voltage FB is set to 1.25 V (typ.). A soft start operates at the time of starting. Positive Charge Pump A controller circuit for the positive-side charge pump. The switching amplitude is controlled so that the feedback voltage FBP will be set to 1.25 V (typ.). Negative Charge Pump A controller circuit for the negative-side charge pump. The switching amplitude is controlled so that the feedback voltage FBN will be set to 0.265 V (Typ.). · Gate Shading Controller A controller circuit for P-MOS FET Switch The GSOUT switching synchronize with CTL input. Please input voltage below VIN to CTL. When VIN drops below UVLO threshold or RST=Low(=RSTIN<1.25V), GSOUT is pulled High(=SRC). VCOM 1-channel operational amplifier block. Reset An open-drain output(RST) refer from RSTIN voltage(up to threshold voltage 1.25V). RST keeps High(need a pull-up resistor connected to VIN) dulling to 185ms from start-up. VREF A block that generates internal reference voltage of 1.25V (Typ.). VREF is keep High when the thermal/short-current-protection shutdown circuit. TSD/UVLO/OVP/UVP The thermal shutdown circuit is shut down at an IC internal temperature of 160°C. The under-voltage lockout protection circuit shuts down the IC when the VIN is 1.85 V (Typ.) or below. The over-voltage protection circuit when the AVDD is 20 V (Typ.) or over. The under-voltage protection circuit when the AVDD is 1.3 V (Typ.) or under Start-up Controller A control circuit for the starting sequence. Controls to start in order of VIN →VGL →AVDD→SRC (Please refer to Fig.27 of 16 page for details.)

#### ●Absolute Maximum Ratings(Ta= 25°C)

PARAMETER	SANDOI	SYNBOL		LIMITS		
PARAWETER	STNDOL	MIN	TYP	MAX	Unit	
Power Supply Voltage	VIN	-0.3	-	7	V	
	AVDD, SW, DRP, DRN, VCOM	-0.3	-	20	V	
	SRC, GSOUT, RE	-0.3	-	36	V	
Output Pin	RST, COMP, VREF	-0.3	-	7	V	
	SRC – GSOUT	-0.3	-	40	V	
Incut Dia	FB, FBP, FBN	-0.3	-	VIN+0.3	V	
Input Pin	INN, INP	-0.3	-	20	V	
Function Pin Voltage	RSTIN, DLY, CTL	-0.3		VIN+0.3	V	
Maximum Junction Temperature	Tjmax	-	-	150	°C	
Operating Temperature Range	Topr	-40	-	105	°C	
Storage Temperature Range	Tstg	-55	-	150	°C	

## ●Thermal Resistance<sup>(Note 2)</sup>

Darameter		Thermal Res	l lucit	
Parameter	Symbol	1s <sup>(Note 4)</sup>	2s2p <sup>(Note 5)</sup>	Unit
VQFN24SV4040	L			
Junction to Ambient	$\theta_{JA}$	150.6	37.9	°C/W
Junction to Top Characterization Parameter <sup>(Note 3)</sup>	$\Psi_{JT}$	20	9	°C/W

(Note 2)Based on JESD51-2A(Still-Air). (Note 3)The thermal characterization parameter to report the difference between junction temperature and the temperature at the top center of the outside surface of the component package.

(NOLE 4)USING A FOB DUALU DAS	ed oll JEOD21-2	-
Layer Number of Measurement Board	Material	Board Size
Single	FR-4	114.3mm x 76.2mm x 1.57mmt
Тор		
Copper Pattern	Thickness	
Footprints and Traces	70µm	

#### (Note 5)Using a PCB board based on JESD51-5, 7.

Layer Number of	Material	Board Size	2	Thermal \	/ia <sup>(Note 6)</sup>
Measurement Board	Material	Doard Size	5	Pitch	Diameter
4 Layers	FR-4	114.3mm x 76.2mm	x 1.6mmt	1.20mm	Ф0.30mm
Тор		2 Internal Layers		Botto	om
Copper Pattern	Thickness	Copper Pattern Thickness		Copper Pattern	Thickness
Footprints and Traces	70µm	74.2mm x 74.2mm	m x 74.2mm 35µm 74.2mm x 74.2mm		n 70µm

(Note 6) This thermal via connects with the copper pattern of all layers.

#### Recommended Operating Range

Parameter	Symbol	MIN	TYP	MAX	Unit
Power Supply Voltage	VIN	2.0	-	5.5	V
Output Bin	AVDD	6	-	18	V
Output Pin	SRC	12	-	34	V

## ●Electrical characteristics (unless otherwise specified VIN = 3.3V, AVDD = 10V and Ta=25°C)

		Limits			u 20 0)	
Parameter	Symbol	Min	Тур	Max	Unit	Condition
GENERAL				L	I	
Circuit Current	I <sub>VIN</sub>	-	1.2	3	mA	No Switching Ta=-40~105°C
Under Voltage Lockout Threshold	V <sub>UVLO</sub>	1.75	1.85	1.95	V	VIN rising Ta=-40~105°C
Internal Reference Output	VREF	1.225	1.25	1.275	V	No load Ta=25°C
Voltage		1.2125	1.25	1.2875	V	No load Ta=-40∼105°C
Thermal Shutdown (rising)	TSD	-	160	-	°C	Junction Temp
Duration to Trigger Fault Condition	T <sub>SCP</sub>	51	63	75	ms	FB , FBP or FBN below threshold
BOOST CONVERTER (AVDD)						
FB Regulation Voltage	V <sub>FB</sub>	1.2375	1.25	1.2625	V	Ta=25°C
	•16	1.2125	1.25	1.2875	V	Ta=-40∼105°C
FB Fault Trip Level	$V_{TL\_FB}$	0.9	1.0	1.1	V	FB falling
FB Input Bias Current	I <sub>FB</sub>	-	0.1	2	μA	FB= 1.5V Ta=-40~105°C
SW Leakage Current	I <sub>SW_L</sub>	-	0	10	μA	SW=20V Ta=-40~105°C
Maximum switching Duty Cycle	MDUTY	85	90	95	%	FB= 1.0V
SW ON-Resistance	R <sub>sw</sub>	-	200	250	mΩ	SW= 200mA
SW Current Limit	I <sub>SWLIM</sub>	2.5	4.5	6.5	А	Ta=-40∼105°C
Over Voltage Protection	V <sub>OVP</sub>	18	20	22	V	AVDD rising
Under Voltage Protection	V <sub>UVP</sub>	1	1.3	3	V	AVDD falling
BOOST Soft Start Time	$T_{SS_{FB}}$	12.5	15.5	18.5	ms	Ta=-40∼105°C
Oscillator frequency	Fsw	1.9	2.1	2.3	MHz	Ta=25°C
		1.88	2.1	2.32	MHz	Ta=-40∼105°C
RESET						
RST Output Low Voltage	V <sub>RST</sub>	-	0.05	0.2	V	RST =1.2mA RSTIN rising
RSTIN Threshold Voltage	V <sub>TH_L</sub>	1.18	1.25	1.32	V	Ta=-40~105°C RSTIN=0 to VIN-0.3
RSTIN Input Current	I <sub>RSTIN</sub>	-	0	6	μA	Ta=-40~105°C
RST Blanking Time	$T_{NO\_SCP}$	165	185	205	ms	No SCP Zone Ta=-40~105°C
Operational Amp rifer						
Input Range	V <sub>RANGE</sub>	0	-	AVDD	V	
Offset Voltage	V <sub>os</sub>	-	2	15	mV	INP= 5.0V
Input Current	I <sub>INP</sub>	-	0	3	μA	INP= 5.0V Ta=-40~105°C
Output Swing Voltage	V <sub>OH</sub>	-	5.03	5.06	V	VCOM = +50mA
(INP= 5.0V)	V <sub>OL</sub>	4.94	4.97	-	V	VCOM = -50mA
Short Circuit Current	I <sub>SHT_VCOM</sub>	-	200	400	mA	INP= 5.0V
Slew Rate	SR	10	40	250	V/us	

## ● Electrical characteristics (unless otherwise specified VIN = 3.3V, AVDD = 10V and Ta=25°C) (Continued)

	Symbol		Limits			
Parameter	Symbol	Min	Тур	Max	Unit	Condition
Negative Charge pump driver (VGI	_)	I				
		242	265	288	mV	Ta=25°C
FBN Regulation Voltage	V <sub>FBN</sub>	239	265	291	mV	Ta=-40~105°C
FBN Fault Trip Level	V <sub>TL_FBN</sub>	400	450	500	mV	FBN rising
FBN Input Bias Current	I <sub>FBN</sub>	-	0.1	15	μA	FBN= 0.1V Ta=-40~105°C
Oscillator frequency	F <sub>CPN</sub>	425	525	625	kHz	Ta=-40~105°C
DRN Leakage Current	I <sub>DRN_L</sub>	-	0	10	μA	FBN=1.0V Ta=-40~105°C
Positive Charge pump driver (SRC	)					
FBP Regulation Voltage	V <sub>FBP</sub>	1.2325	1.25	1.2675	V	Ta=25°C
T BF Regulation voltage	V FBP	1.2125	1.25	1.2875	V	Ta=-40~105°C
FBP Fault Trip Level	$V_{TL\_FBP}$	0.95	1.0	1.05	V	FBP falling
FBP Input Bias Current	I <sub>FBP</sub>	-	0.1	15	μA	FBP= 1.5V Ta=-40~105°C
Oscillator frequency	F <sub>CPP</sub>	425	525	625	kHz	Ta=-40~105°C
DRP Leakage Current	I <sub>DRP_L</sub>	-	0	10	μA	FBP= 1.5V Ta=-40~105°C
Soft-Start Time	T <sub>SSP</sub>	3.2	3.9	4.6	ms	Ta=-40~105°C
Gate Shading Function (GSOUT)						
DLY Source Current	I <sub>DLY</sub>	3.5	5	6.5	μA	Ta=-40~105°C
DLY Threshold Voltage	V <sub>TL_DLY</sub>	0.85	1.25	1.65	V	DLY falling Ta=-40~105°C
CTL Input Voltage High	V <sub>IN_H</sub>	VIN × 0.65	-	VIN	V	Depend on VIN Ta=-40~105°C
CTL Input Voltage Low	V <sub>IN_L</sub>	0	-	VIN × 0.25	V	Depend on VIN Ta=-40~105°C
CTL Input Bias Current	ICTL	-	0	6	μA	RSTIN=0 to VIN-0.3 Ta=-40~105℃
Propagation delay time (Rising)	T <sub>GS_R</sub>	-	100	200	ns	SRC= 25V
Propagation delay time (Falling)	T <sub>GS_F</sub>	-	100	200	ns	SRC= 25V
SRC -GSOUT ON Resistance	R <sub>GS_H</sub>	-	15	30	Ω	DLY = 1.5V
GSOUT-RE ON Resistance	R <sub>GS_M</sub>	-	30	100	Ω	DLY = 1.5V
GSOUT-GND ON Resistance	R <sub>GS_L</sub>	-	2.5	5.0	kΩ	DLY = 1.0V

OThis product is not designed for protection against radio active rays.



#### •Electrical characteristic curves (Reference data)





Figure 10. Boost Converter Efficiency



Figure 11. COMP V.S.DUTY

#### •Electrical characteristic curves (Reference data)



## Electrical characteristic curves (Reference data) – Continued





Figure 18. C\_DLY vs. delay time

## Electrical characteristic curves (Reference data) – Continued



Figure 19. Gate Shading Wave form1



Figure 20. Gate Shading Wave form2









## ●Electrical characteristic curves (Reference data) – Continued



Figure 23. Power Off Sequence2 (R\_RST\_U=10k,R\_RST\_D=10k)



Figure 24. Power Off Sequence3 (R\_RST\_U=10k,R\_RST\_D=OPEN)



Figure 25. Power On Sequence2 (CTL=signal, RE pull down to AVDD)

## Application Example



Parts		Value			Company	Parts Number
name	Min	Тур	Max	Unit	Company	
C_VIN	0.47	1.0	-	uF	TDK	CGA3E1X7R1C105M
R_VIN	1	10	20	Ω	ROHM	MCR03
C_PIN1	4.7	10	-	uF	TDK	CGA5L1X7R1C106M
C_PIN2	4.7	10	-	uF	TDK	CGA5L1X7R1C106M
C_AVD1	4.7	10	22	uF	TDK	CGA5L1X7R1E106M
C_AVD2	4.7	10	22	uF	TDK	CGA5L1X7R1E106M
L_AVD	4.7	10	22	uH	TDK	LTF5022T-100M1R3-H
D_AVD	-	30/5	-	V/A	ROHM	RB080L-30DD
R_AVD_U	6.8	91	330	kΩ	ROHM	MCR03
R_AVD_D	6.8	13	330	kΩ	ROHM	MCR03
R_CMP	-	24	-	kΩ	ROHM	MCR03
C_CMP	-	2200	-	pF	TDK	CGA3E2X7R1H222M
R_RST_U	-	10	-	kΩ	ROHM	MCR03
R_RST_D	-	10	-	kΩ	ROHM	MCR03
R_RST	-	10	-	kΩ	ROHM	MCR03
C_RST	-	1.0	-	uF	TDK	CGA3E1X7R1C105M
C_DLY	10	33	100	nF	TDK	CGA3E2X7R1H333M
R_RE	0.2	1.0	5.1	kΩ	ROHM	MCR03
C_AVDD	0.047	0.1	-	uF	TDK	CGA3E2X7R1H104M
C_REF	0.1	0.22	0.47	uF	TDK	CGA3E2X7R1C224M

Parts		Value		Linit	Compony	Parts Number	
name	Min	Тур	Max	Unit	Company		
C_VGL	0.47	1.0	10	uF	TDK	CGA3E1X7R1C105M	
C_FCN	0.047	0.1	1.0	uF	TDK	CGA3E2X7R1H104M	
D_CPN	-	80/100	-	V/mA	ROHM	DAN217UMFH	
R_VGL_U	6.8	120	330	kΩ	ROHM	MCR03	
R_VGL_D	6.8	16	330	kΩ	ROHM	MCR03	
C_VGL_U	10	100	4700	pF	TDK	CGA3E2NP01H101J	
C_SRC1	0.47	1.0	10	uF	TDK	CGA4J3X7R1H105M	
C_FCP1	0.047	0.1	1.0	uF	TDK	CGA3E2X7R1H104M	
C_FCP2	0.047	0.1	1.0	uF	TDK	CGA3E2X7R1H104M	
C_CPP	0.047	0.1	1.0	uF	TDK	CGA3E2X7R1H104M	
D_CPP1	-	80/100	-	V/mA	ROHM	DAN217UMFH	
D_CPP2	-	80/100	-	V/mA	ROHM	DAN217UMFH	
R_SRC_U	6.8	150	330	kΩ	ROHM	MCR03	
R_SRC_D	6.8	10	330	kΩ	ROHM	MCR03	
C_SRC_U	10	100	4700	pF	TDK	CGA3E2NP01H101J	
C_SRC2	0.47	1.0	10	uF	TDK	CGA4J3X7R1H105M	
R_COM_U	6.8	51	330	kΩ	ROHM	MCR03	
R_COM_D	6.8	51	330	kΩ	ROHM	MCR03	
C_VCOM	0.1	1.0	10	uF	TDK	CGA3E1X7R1E105M	

%Please set in consideration of temperature properties and DC bias properties not to become less than the minimum. COMP parts and the coil need adjustment by output voltage and load. Please consider it based on enough evaluations with the actual model.

#### Power Sequence





## Protect Operation

VIN UVLO

	AVDD	SRC	VGL
Falling (Typ.)	1.65V		
Rising (Typ.)	1.85V		
Action	All channels shut-down. Start-up Sequence Resets.		

#### Thermal Shutdown

	AVDD	SRC	VGL
Threshold (Typ.)	160°C		
Action	All channels are latched in shut-down condition as soon as detecting Thermal Shutdown. For Recovery, power supply should be inputted under UVLO voltage.		

#### Over Voltage Protection

	AVDD	
Threshold (Typ.)	20V	
Action	STOP switching of AVDD.	

#### Under Voltage Protect

<b>0</b>		
	AVDD	
Threshold (Typ.)	1.3V	
Action	STOP switching of AVDD.	

#### Over Current Protect

	AVDD	
Threshold (Min.)	2.5A	
Action	STOP switching of AVDD.	

#### Short Circuit Protect

	AVDD	SRC	VGL
Threshold (Typ.)	AVDD x 0.8	SRC x 0.8	VGL x 0.8
Action	All channels are latched in shut-down condition after 63msec(Typ.) detecting Short Circuit Protect in any channel. For Recovery, power supply should be inputted under UVLO voltage.		

## Reset Function



The RST is set to Low when the RSTIN voltage is less than 1.25V and is set to High (pulled-up by a resistor to VIN) when the RSTIN voltage is greater than or equal to 1.25V. However, during the time when power supply is ON for 185ms (Typ), RST is held High regardless of RSTIN voltage.

Gate Shading function is activated when RST\_EN is High. When RSTIN is Low, the Gate Shading function cannot be used. If the Gate Shading function will not be used, the SRC, RE, and CTL must be pulled-down by a resistor or connected to GND.

## Gate Shading Function



To control the Gate Shading output (GSOUT) by the CTL input, the RSTIN and DLY pin voltages must be set greater than 1.25V. If the DLY pin is left open, the DLY voltage immediately becomes High (greater than 1.25V) when the power supply is turned ON. To add a delay time (t\_DELAY) before DLY voltage becomes High, connect a capacitor (C\_DLY) to the DLY pin The delay time (t\_DELAY) can be calculated using the following formula.

$$t_DELAY = (C_{DLY} \times 1.25V)/5uA$$
 [sec]

When the CTL input is High (0.65 × VIN to VIN), the MOS between SRC and GSOUT turns ON and sets the output voltage of GSOUT equal to SRC.

When the CTL input is Low (0 to 0.25 × VIN), the MOS between GSOUT and RE turns ON, and GSOUT will be discharged down to RE voltage by a slope decided by the external resistor (R\_RE) and capacitor (C\_GSO).

To adjust a slope, the following setting value is recommended; for resistor (R\_RE):200  $\Omega$  - 5.1k $\Omega$ , for capacitor (C\_GSO):less than 0.1uF. It may cause the efficiency aggravation by setting out of this range.

The voltage ΔV that GSOUT discharges during the time (t\_WL) when CTL input is Low can be calculated using the following formula.

$$\Delta V = SRC \times \left(1 - exp\left(-\frac{t\__{WL}}{C\__{GSO} \times R\__{RE}}\right)\right) \qquad [V]$$

But the loss occurs when C\_GSO is added. The loss  $\Delta P$  can be calculated using the following formula.

$$\Delta P = Frequency(CTL) \times \Delta V^2 \times C_{GSO}$$
 [V]



If the Gate Shading function will not be used, the SRC, RE, and CTL must be pulled-down by a resistor or connected to GND. And the DLY, please connect capacitor because there is the concern such as noises.

## How to select parts of application



Adjust so that INMAX + $\Delta$ IL does not reach the rating current value ILR. In addition, become the Discontinuous Condition Mode (DCM) when IL reaches 0mA. As for the section which DCM and Continuous Condition Mode (CCM) are replaced by, jitter properties turn worse. Adjust the coil so that INMAX - $\Delta$ IL does not reach the 0mA.  $\Delta$ IL can be obtained by the following equation.

$$\Delta I_{L} = \frac{1}{L} \quad VIN \times \frac{AVDD - VIN}{AVDD} \times \frac{1}{f} \qquad [A] \quad \text{Here, f is the switching frequency.}$$

Set with sufficient margin because the coil value may have the dispersion of  $\pm 30\%$ . If the coil current exceeds the rating current ILR of the coil, it may damage the IC internal element.

BD81842MUV-M uses the current mode DC/DC converter control and has the optimized design at the coil value. A coil inductance (L) of 4.7 uH to 22 uH is recommended from viewpoints of electric power efficiency, response, and stability.

## (2) Output Capacity Settings

For the capacitor to use for the output, select the capacitor which has the larger value in the ripple voltage VPP allowance value and the drop voltage allowance value at the time of sudden load change. Output ripple voltage is decided by the following equation.

$$\Delta V_{PP} = I_{LMAX} \times RESR + \frac{1}{fCo} \times \frac{VIN}{AVDD} \times (I_{LMAX} - \frac{\Delta I_{L}}{2}) [V]$$
Here, f is the switching frequency  
and RESR is ESR of output capacitor.

Perform setting so that the voltage is within the allowable ripple voltage range. For the drop voltage during sudden load change; VDR, please perform the rough calculation by the following equation.

$$V_{DR} = \frac{\Delta I}{Co} \times 10 \text{ us}$$
 [V]

However, 10  $\mu$ s is the rough calculation value of the DC/DC response speed. Please set the capacitance considering the sufficient margin so that these two values are within the standard value range.

## (3) Selecting the Input Capacitor

Since the peak current flows between the input and output at the DC/DC converter, a capacitor is required to install at the input side. For the reason, the low ESR capacitor is recommended as an input capacitor which has the value more than 10  $\mu$ F and less than 100 m $\Omega$ . If a capacitor out of this range is selected, the excessive ripple voltage is superposed on the input voltage, accordingly it may cause the malfunction of IC.

However these conditions may vary according to the load current, input voltage, output voltage, inductance and switching frequency. Be sure to perform the margin check using the actual product.

#### (4) Setting Rc, Cc of the Phase Compensation Circuit

In the current mode control, since the coil current is controlled, a pole (phase lag) made by the CR filter composed of the output capacitor and load resistor will be created in the low frequency range, and a zero (phase lead) by the output capacitor and ESR of capacitor will be created in the high frequency range. In this case, to cancel the pole of the power amplifier, it is easy to compensate by adding the zero point with Cc and Rc to the output from the error amp as shown in the illustration.

#### **Open loop gain characteristics**











Figure 34. Application Circuit Diagram

 $fz(ESR) = \frac{1}{2 \pi \times ESR \times CO}$ [Hz] Pole at the power amplification stage

 $Fp = \frac{1}{2 \pi \times Ro \times Co} [Hz]$ 

When the output current reduces, the load resistance  $\mathsf{R}_0$  increases and the pole frequency lowers.

$$fp(Min) = \frac{1}{2 \pi \times ROMax \times CO} [Hz] \leftarrow at light load$$
$$fz(Max) = \frac{1}{2 \pi \times ROMin \times CO} [Hz] \leftarrow at heavy load$$

#### Zero at the power amplification stage

When the output capacitor is set larger, the pole frequency lowers but the zero frequency will not change. (This is because the capacitor ESR becomes 1/2 when the capacitor becomes 2 times.)

$$fp(Amp.) = \frac{1}{2 \pi \times Rc \times Cc} \quad [Hz]$$

It is possible to realize the stable feedback loop by canceling the pole fp(Min.), which is created by the output capacitor and load resistor, with CR zero compensation of the error amp as shown below.

$$fz(Amp.) = fp(Min.)$$

$$\xrightarrow{1} \frac{1}{2 \pi \times Rc \times Cc} = \frac{1}{2 \pi \times Romax \times Co}$$
[Hz]

## (5) Design of the Feedback Resistor Constant

Refer to the following equation to set the feedback resistor. As the setting range, 6.8 k $\Omega$  to 330 k $\Omega$  is recommended. If the resistor is set lower than a 6.8 k $\Omega$ , it causes the reduction of power efficiency. If it is set more than 330 k $\Omega$ , the offset voltage becomes larger by the input bias current 0.1  $\mu$ A(Typ.) in the internal error amplifier.



Figure 35. Application Circuit Diagram

## (6) Positive-side Charge Pump Settings

The IC incorporates a charge pump controller, thus making it possible to generate stable gate voltage. The output voltage is determined by the following formula. As the setting range, 6.8 k $\Omega$  to 330 k $\Omega$  is recommended. If the resistor is set lower than a 6.8k $\Omega$ , it causes the reduction of power efficiency. If it is set more than 330 k $\Omega$ , the offset voltage becomes larger by the input bias current 0.1  $\mu$ A (Typ.) in the internal error amp.



In order to prevent output voltage overshooting, add capacitor C\_SRC\_U in parallel with R\_SRC\_U. The recommended capacitance is 10 pF to 4700 pF. But please enough evaluate with the actual model because adjustments in the application may be necessary.

Please meet the following condition about the number of the steps of the charge pump. In addition, confirm with an actual model for the last time. Because the loss is increase when a calculation result is the small, please be careful.

$$\frac{SRC}{(n+1)x \text{ AVDD } - 2n x \text{ Vf}} < 1$$
 Here, n is the steps of charge pump, Vf is the forward voltage of diode.

(7) Negative-side Charge Pump Settings

This IC incorporates a charge pump controller for negative voltage, thus making it possible to generate stable gate voltage.

The output voltage is determined by the following formula. As the setting range, 6.8 k $\Omega$  to 330 k $\Omega$  is recommended. If the resistor is set lower than a 6.8 k $\Omega$ , it causes the reduction of power efficiency. If it is set more than 330 k $\Omega$ , the offset voltage becomes larger by the input bias current 0.1  $\mu$ A (Typ.) in the internal error amp.



Figure 37. Application Circuit Diagram

In order to prevent output voltage overshooting, insert capacitor C\_VGL\_U in parallel with R\_VGL\_U. The recommended capacitance is 10 pF to 4700 pF. But please enough evaluate with the actual model because adjustments in the application may be necessary.

Please meet the following condition about the number of the steps of the charge pump. In addition, confirm with an actual model for the last time. Because the loss is increase when a calculation result is the small, please be careful.

Here,  $\ensuremath{\mathsf{n}}$  is the steps of charge pump, Vf is the forward voltage of diode.

(8) VCOM Amplifier block

VCOM Amplifier is a rail-to-rail high slew rate Operational Amplifier which has 0V - AVDD voltage (the 1pin (INP) input voltage) as an input and output voltage range.

When add a capacitor to output, 0.1uF – 10uF is recommended for the reason of stability.



Figure 38. Application Circuit Diagram

## BD81842MUV-M

#### (9) Process of unused function

When Gate Shading Function is not used, please proceed each pin (SRC, RE, CTL, DLY) as follows.



Figure 39. Application Circuit

When VCOM function is not used, please proceed each pin (INP, INN, VCOM) as follows.



#### ●PCB Layout Guide

#### **GND Wiring Pattern**

The high current GND (PGND) should be wired thick. To reduce line impedance, the GND lines must be as short and thick as possible and uses few via. Therefore design at PCB board four layers or above is recommended. (Please use the middle layer as GND shielding and directly connect each GND.) In the case of two layers or less at PCB board designs, please enough confirm with the actual model about the heat and the noise with care to a GND wiring.

#### Switching-Line Wiring Pattern

The wiring from switching line (SW pin) of DC/DC converter to inductor and diode must be as short and thick as possible. If a wiring is long, ringing by switching increases, and the voltage over the resistance of this IC might be generated. Please note that switching line does not vary PCB layer.

Switching line and wiring easily affected by noise such as feedback line or COMP line must be placed separately. Switching noise spread may cause the lack of operation stability. In case the multi-layer PCB board, please note that a switching line and a line easily affected by noise or the external components are not adjacent between layers. Drawing GND shield line between switching line and these lines easily affected by noise is recommended if these lines are placed close.

#### **Power Supply Voltage Line Wiring Pattern**

For power supply voltage (VIN) and internal reference voltage (VREF), place smooth capacitor nearby IC pin. Especially, VIN is a power supply line of internal MOSFET for Boost DC/DC, placing capacitor at distance within 2mm from pin is needed. In addition, wire the VIN line by thickness more than 3mm.

Furthermore, insert the resistance (RC filter formation) on VIN line and become stronger in a power supply change. Please note that smooth capacitor does not vary PCB layer.

The figure 41 shows an application circuit on the basis of the basic PCB layout pattern guideline mentioned above.

- Bold line: High current line
- Blue line(two dots and dashed line): Wiring easily affected by noise
- Red line (dashed line): Noise source line such as switching line



#### **Recommended Layout Pattern**



Figure 42. Recommended Layout Pattern

#### **EMC Layout Guide**

Introduce the plan that can design on the PCB as EMC measures.

Measures by the board pattern

- ① Wire AVDD line briefly thickly.
- ② Wire the current loop of Boost DC/DC briefly thickly.

Measures by the external component

- ③ Insert a common mode filter or a beads coil in the AVDD line and form the EMC filter.
- ④ Place output capacitor and small capacitor (10pF 1,000pF) in parallel.
- (5) Insert the snubber circuit in SW pin. (Assumed the efficiency becomes worse)



Figure 43. Application Circuit



Figure 44. Current loop

## ●I/O Equivalent Circuit Diagrams

(Except for 4.AGND1, 14.AGND2, 18.PGND1, 19.PGND2)



#### Operation Notes

#### 1. Reverse Connection of Power Supply

Connecting the power supply in reverse polarity can damage the IC. Take precautions against reverse polarity when connecting the power supply, such as mounting an external diode between the power supply and the IC's power supply pins.

#### 2. Power Supply Lines

Design the PCB layout pattern to provide low impedance supply lines. Separate the ground and supply lines of the digital and analog blocks to prevent noise in the ground and supply lines of the digital block from affecting the analog block. Furthermore, connect a capacitor to ground at all power supply pins. Consider the effect of temperature and aging on the capacitance value when using electrolytic capacitors.

#### 3. Ground Voltage

Ensure that no pins are at a voltage below that of the ground pin at any time, even during transient condition.

#### 4. Ground Wiring Pattern

When using both small-signal and large-current ground traces, the two ground traces should be routed separately but connected to a single ground at the reference point of the application board to avoid fluctuations in the small-signal ground caused by large currents. Also ensure that the ground traces of external components do not cause variations on the ground voltage. The ground lines must be as short and thick as possible to reduce line impedance.

#### 5. Thermal Consideration

Should by any chance the power dissipation rating be exceeded the rise in temperature of the chip may result in deterioration of the properties of the chip. In case of exceeding this absolute maximum rating, increase the board size and copper area to prevent exceeding the Pd rating.

#### 6. Recommended Operating Conditions

These conditions represent a range within which the expected characteristics of the IC can be approximately obtained. The electrical characteristics are guaranteed under the conditions of each parameter.

#### 7. Inrush Current

When power is first supplied to the IC, it is possible that the internal logic may be unstable and inrush current may flow instantaneously due to the internal powering sequence and delays, especially if the IC has more than one power supply. Therefore, give special consideration to power coupling capacitance, power wiring, width of ground wiring, and routing of connections.

#### 8. Operation Under Strong Electromagnetic Field

Operating the IC in the presence of a strong electromagnetic field may cause the IC to malfunction.

#### 9. Testing on Application Boards

When testing the IC on an application board, connecting a capacitor directly to a low-impedance output pin may subject the IC to stress. Always discharge capacitors completely after each process or step. The IC's power supply should always be turned off completely before connecting or removing it from the test setup during the inspection process. To prevent damage from static discharge, ground the IC during assembly and use similar precautions during transport and storage.

#### 10. Inter-pin Short and Mounting Errors

Ensure that the direction and position are correct when mounting the IC on the PCB. Incorrect mounting may result in damaging the IC. Avoid nearby pins being shorted to each other especially to ground, power supply and output pin. Inter-pin shorts could be due to many reasons such as metal particles, water droplets (in very humid environment) and unintentional solder bridge deposited in between pins during assembly to name a few.

#### 11. Unused Input Pins

Input pins of an IC are often connected to the gate of a MOS transistor. The gate has extremely high impedance and extremely low capacitance. If left unconnected, the electric field from the outside can easily charge it. The small charge acquired in this way is enough to produce a significant effect on the conduction through the transistor and cause unexpected operation of the IC. So unless otherwise specified, unused input pins should be connected to the power supply or ground line.

## **Operational Notes – continued**

#### 12. Regarding the Input Pin of the IC

This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated. P-N junctions are formed at the intersection of the P layers with the N layers of other elements, creating a parasitic diode or transistor. For example (refer to figure below):

When GND > Pin A and GND > Pin B, the P-N junction operates as a parasitic diode. When GND > Pin B, the P-N junction operates as a parasitic transistor.

Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, operational faults, or physical damage. Therefore, conditions that cause these diodes to operate, such as applying a voltage lower than the GND voltage to an input pin (and thus to the P substrate) should be avoided.



Figure 45. Example of monolithic IC structure

#### 13. Ceramic Capacitor

When using a ceramic capacitor, determine the dielectric constant considering the change of capacitance with temperature and the decrease in nominal capacitance due to DC bias and others.

#### 14. Area of Safe Operation (ASO)

Operate the IC such that the output voltage, output current, and power dissipation are all within the Area of Safe Operation (ASO).

#### 15. Thermal Shutdown Circuit(TSD)

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. Normal operation should always be within the IC's power dissipation rating. If however the rating is exceeded for a continued period, the junction temperature (Tj) will rise which will activate the TSD circuit that will turn OFF all output pins. When the Tj falls below the TSD threshold, the circuits are automatically restored to normal operation.

Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.

#### 16. Over Current Protection Circuit (OCP)

This IC incorporates an integrated overcurrent protection circuit that is activated when the load is shorted. This protection circuit is effective in preventing damage due to sudden and unexpected incidents. However, the IC should not be used in applications characterized by continuous operation or transitioning of the protection circuit.

## Ordering Information



#### Marking Diagrams



#### Physical Dimension, Tape and Reel Information VQFN24SV4040 Package Name 4. 0±0. 1 0=0. 4 1 PIN MARK 0MAX 80 22 0 2 + 0 ○0.08 S 9 d 4±0.1 2 C0. 2 U 24 ó # -4±0. e i ó 19 ጠጠ n $\cap$ 18 13 75 0. $0.25^{+0.05}_{-0.04}$ 0. 5 <Tape and Reel information> Embossed carrier tape Таре Quantity 2500pcs E2 Direction (The direction is the 1pin of product is at the upper left when you hold reel on the left hand and you pull out the tape on the right hand of feed 0 0 0 0 Ο Ο Ο Ο Ο Ο Ο Ο Direction of feed 1pin Reel \*Order quantity needs to be multiple of the minimum quantity.

## Revision History

Date	Revision	Changes
07.Sep.2015	001	New Release
23.Jun.2016	002	<ul> <li>①P6 Thermal Resistance : Footprints and Traces 74.2mm<sup>2</sup>(Square) ⇒ 74.2mm x 74.2mm</li> <li>②P25 Add Recommended Layout Pattern</li> </ul>

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JAPAN	USA	EU	CHINA
CLASSI	CLASSI	CLASS II b	CLASSII
CLASSⅣ		CLASSⅢ	CLASSII

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  - [h] Use of the Products in places subject to dew condensation
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